

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 22.03.2018

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OWASpKonErgAus	Sco	Prz	Bd	NS	OWASpKonErgAus	Sco	Prz
1	7	102	W 4P =	CD -420	5	5	7	112 W 4C +1	P10 -450	36	10	5	105 W 3SA -1	C8 100	32
1	2	103	W 4P =	CD -420	5	5	5	107 W 4C +1	P10 -450	36	10	4	103 O 2SA -1	T5 100	32
1	12	112	W 3P =	CD -140	36	5	6	109 W 3SA +1	P2 -430	82	10	2	111 O 3SA -1	T7 100	32
1	10	108	W 2P +1	CD -140	36	5	4	105 W 4C =	K3 -420	91	10	9	102 W 2P -1	K10 100	32
1	8	104	W 3P =	CD -140	36	5	3	103 W 6C -1	P10 50	100	10	3	101 O 2C -2	P8 200	77
1	6	111	W 2P +1	CD -140	36	6	11	108 O 3SA +3	C9 -690	0	10	1	109 O 3SA -2	T5 200	77
1	4	107	W 2P +1	C4 -140	36	6	3	103 O 3SA +2	C9 -660	9	10	11	106 O 4C -2	T6 200	77
1	9	106	W 2P =	CD -110	64	6	8	102 O 3SA +1	C2 -630	18	10	10	104 O 3SA -2	T7 200	77
1	1	101	N 4C -2	TA -100	73	6	12	110 O 3SA =	C9 -600	27	10	8	112 W 2P -2	C8 200	77
1	3	105	W 4C -1	CD 50	82	6	4	105 N 4P X -3	CA -500	36	10	7	110 W 3SA -2	K10 200	77
1	11	110	W 4P -2	CD 100	95	6	9	104 O 2SA +4	KB -240	45	11	3	112 O 3SA +4	P5 -520	0
1	5	109	W 3P -2	CD 100	95	6	2	101 O 2SA +2	P2 -180	55	11	6	106 W 3SA +2	K6 -460	50
2	7	102	O 4C =	PA -420	5	6	6	109 N 3P -3	T4 -150	68	11	5	104 W 3SA +2	T4 -460	50
2	3	105	O 4C =	PA -420	5	6	5	107 N 2P -3	T9 -150	68	11	4	102 W 3SA +2	T2 -460	50
2	8	104	O 3SA =	K6 -400	18	6	10	106 W 2T +2	PD -130	82	11	2	110 W 3SA +2	T2 -460	50
2	6	111	O 2SA +1	T2 -150	27	6	1	111 W 3T =	PD -110	91	11	1	108 W 3SA +2	P5 -460	50
2	12	112	W 3C =	TA -140	36	6	7	112 N 2P -1	T4 -50	100	11	12	107 W 3SA +2	T2 -460	50
2	2	103	N 2P -1	KA -100	45	7	9	103 O 4C =	PK -620	0	11	10	103 W 3SA +2	P9 -460	50
2	1	101	W 4C -1	TA 50	64	7	3	102 O 5C -1	PK 100	18	11	9	101 W 3SA +2	T2 -460	50
2	11	110	O 1K -1	C4 50	64	7	12	109 W 3T -1	P10 100	18	11	8	111 W 3SA +2	T2 -460	50
2	9	106	W 4C -1	TA 50	64	7	11	107 O 4C -1	KB 100	18	11	7	109 W 3SA +2	T2 -460	50
2	5	109	O 3SA -2	K7 100	82	7	6	108 S 3P +1	TK 170	36	11	11	105 O 4C =	PD -420	100
2	10	108	N 2P =	KA 110	91	7	8	101 S 3P +2	TK 200	50	12	6	106 O 3P =	CD -140	9
2	4	107	N 2P +2	KA 170	100	7	5	106 S 3P +2	TK 200	50	12	1	108 O 2P +1	CD -140	9
3	11	109	S 2C -1	P2 -50	5	7	4	104 S 4P =	T4 620	73	12	9	101 O 2P +1	KA -140	9
3	5	108	S 2C -1	P2 -50	5	7	2	112 N 4P =	TA 620	73	12	5	104 O 2P =	C8 -110	36
3	7	101	Pass	0	27	7	10	105 S 4P =	C7 620	73	12	8	111 O 2P =	CD -110	36
3	4	106	Pass	0	27	7	1	110 S 4P +1	TK 650	91	12	7	109 O 2P =	CD -110	36
3	3	104	Pass	0	27	7	7	111 N 5P X =	TA 850	100	12	2	110 O 2P -1	C8 50	59
3	12	111	S 2C =	P2 110	59	8	11	107 N 3SA -4	CB -200	0	12	12	107 O 2P -1	T3 50	59
3	10	107	S 2C =	K5 110	59	8	10	105 N 2SA -3	K3 -150	14	12	4	102 O 3P -2	C8 100	73
3	9	105	S 2C =	K8 110	59	8	6	108 N 2C -3	P9 -150	14	12	11	105 S 3C =	P9 140	86
3	8	103	S 2C =	K5 110	59	8	3	102 W 1SA +1	CA -120	36	12	10	103 S 3C =	P9 140	86
3	2	102	S 3C =	K5 140	82	8	1	110 W 1SA +1	CA -120	36	12	3	112 S 3C +1	P5 170	100
3	1	112	S 2C +2	PB 170	91	8	8	101 W 1SA +1	CA -120	36	13	5	103 N 3SA =	P4 600	5
3	6	110	W 2SA -2	C10 200	100	8	5	106 S 2T -2	C7 -100	55	13	7	108 S 3SA =	P9 600	5
4	3	104	S 4P -4	T6 -400	0	8	12	109 N 1SA -1	K3 -50	68	13	4	101 N 3SA +1	P4 630	41
4	7	101	N 3P -3	T10 -300	14	8	7	111 S 2T -1	C6 -50	68	13	1	107 N 3SA +1	P4 630	41
4	4	106	N 4C -3	K4 -300	14	8	4	104 O 3K -1	C8 50	86	13	12	106 N 3SA +1	P4 630	41
4	1	112	N 4C -2	K2 -200	27	8	9	103 W 1SA -1	C9 50	86	13	11	104 N 3SA +1	P4 630	41
4	5	108	O 3T =	C2 -110	36	8	2	112 S 2T +1	C5 110	100	13	9	112 N 3SA +1	T3 630	41
4	11	109	N 3C -1	T8 -100	50	9	2	111 N 4C +2	P10 480	5	13	8	110 N 3SA +1	P4 630	41
4	8	103	S 4C -1	K10 -100	50	9	1	109 N 4C +2	K4 480	5	13	6	105 N 3SA +2	P4 660	86
4	2	102	N 2C =	T3 110	68	9	9	102 S 3SA +3	PD 490	23	13	3	111 N 3SA +2	K5 660	86
4	9	105	S 2P =	TD 110	68	9	7	110 S 3SA +3	P7 490	23	13	2	109 N 3SA +2	P4 660	86
4	12	111	S 3C =	TD 140	86	9	5	105 N 4C +3	P10 510	45	13	10	102 N 3SA +2	P4 660	86
4	10	107	N 2C +1	K4 140	86	9	12	108 N 4C +3	KB 510	45	14	6	105 N 5T X -2	CA -300	0
4	6	110	N 4C =	K4 620	100	9	10	104 N 4C +3	P10 510	45	14	10	102 W 4K =	TK -130	9
5	2	101	W 4C +1	K3 -450	36	9	4	103 N 3SA +4	P10 520	68	14	5	103 N 5T X -1	CA -100	27
5	1	111	W 4C +1	P10 -450	36	9	6	107 S 3SA +4	P7 520	68	14	2	109 N 3SA -2	K2 -100	27
5	12	110	W 5C =	C5 -450	36	9	11	106 N 6C =	P2 980	82	14	7	108 N 4T X -1	K4 -100	27
5	11	108	O 4C +1	T10 -450	36	9	3	101 N 6C +1	C5 1010	95	14	1	107 N 4T -1	K5 -50	45
5	10	106	W 4C +1	P10 -450	36	9	8	112 N 6C +1	P2 1010	95	14	3	111 W 3K -1	TK 50	59
5	9	104	W 4C +1	K3 -450	36	10	6	107 S 3SA -3	C7 -300	0	14	11	104 W 4K -1	TK 50	59
5	8	102	W 4C +1	K8 -450	36	10	12	108 O 2C =	K2 -110	9	14	8	110 N 3T =	K4 110	73

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
14	4	101	N 4T =	K2	130	91	19	5	112 S 4C +2	PK	480	50	23	11	111 S 3SA =	P8	600	100
14	12	106	N 4T =	K5	130	91	19	4	110 S 4C +2	PK	480	50	24	5	110 S 5K X -2	PA	-300	0
14	9	112	N 4T =	K2	130	91	19	3	108 S 5C +1	P5	480	50	24	9	107 W 2P +1	TK	-140	14
15	8	109	O 4C =	T4	-420	0	19	2	106 S 4C +2	PK	480	50	24	2	104 W 1P +2	TK	-140	14
15	2	108	O 2C +2	T10	-170	9	19	1	104 S 4C +2	PK	480	50	24	7	103 W 2P =	TK	-110	41
15	7	107	O 3C =	T7	-140	45	19	11	101 S 4C +2	PK	480	50	24	3	106 W 2P =	K9	-110	41
15	5	102	O 3C =	P2	-140	45	19	10	111 S 4C +2	PK	480	50	24	1	102 W 2P =	K6	-110	41
15	3	110	O 3C =	T5	-140	45	19	12	103 O 4P X -2	T7	500	100	24	12	101 W 2P =	TK	-110	41
15	1	106	O 3C =	T4	-140	45	20	6	102 W 4C +2	T6	-680	5	24	10	109 W 2T =	P8	-90	64
15	12	105	O 3C =	T7	-140	45	20	3	108 W 4C +2	T6	-680	5	24	11	111 W 4P -1	K9	50	77
15	11	103	O 3C =	TK	-140	45	20	5	112 W 4C +1	T6	-650	32	24	4	108 W 3P -1	K4	50	77
15	9	111	O 3C =	TK	-140	45	20	2	106 W 4C +1	T6	-650	32	24	6	112 W 4P -2	TK	100	91
15	6	104	S 3P +1	CK	170	86	20	1	104 W 4C +1	PD	-650	32	24	8	105 S 3K +1	CA	130	100
15	4	112	S 1P +3	T8	170	86	20	12	103 W 4C +1	PD	-650	32						
15	10	101	S 4P =	T8	620	100	20	4	110 W 4C =	P9	-620	55						
16	4	112	N 6P -1	CA	-50	0	20	11	101 W 3C +3	T6	-230	64						
16	7	107	S 3SA +1	C4	430	18	20	9	109 W 2SA +3	PD	-210	73						
16	6	104	S 3SA +1	C4	430	18	20	7	105 S 4K -1	CA	-100	82						
16	9	111	S 3SA +1	C4	430	18	20	8	107 W 4C -1	PD	100	95						
16	8	109	N 4P +1	C9	450	36	20	10	111 W 4C -1	K3	100	95						
16	5	102	S 3SA +2	C4	460	64	21	11	112 N 1SA -3	P10	-300	0						
16	3	110	S 3SA +2	C4	460	64	21	5	111 N 1SA -2	KB	-200	14						
16	2	108	S 3SA +2	C4	460	64	21	2	105 N 1SA -2	K4	-200	14						
16	12	105	S 3SA +2	C4	460	64	21	9	108 O 1SA +3	P5	-180	32						
16	11	103	S 3SA +2	C4	460	64	21	6	101 O 1SA +3	P2	-180	32						
16	1	106	N 3SA +3	C4	490	95	21	8	106 W 2C +2	TK	-170	55						
16	10	101	S 3SA +3	C4	490	95	21	7	104 W 3C +1	PA	-170	55						
17	8	108	S 3P +1	K3	170	0	21	12	102 W 2C +2	TK	-170	55						
17	7	106	N 3SA =	K6	400	9	21	10	110 W 2C +1	P3	-140	77						
17	5	101	S 4P =	T2	420	45	21	4	109 W 2C +1	KK	-140	77						
17	4	111	N 4P =	K8	420	45	21	3	107 W 2C =	PA	-110	95						
17	2	107	S 4P =	K2	420	45	21	1	103 W 2C =	TK	-110	95						
17	12	104	S 4P =	K2	420	45	22	2	105 O 2T =	C9	-90	0						
17	11	102	N 4P =	CK	420	45	22	5	111 S 4P -1	TD	-50	18						
17	10	112	S 4P =	T9	420	45	22	1	103 N 4P -1	TA	-50	18						
17	9	110	S 4P =	K2	420	45	22	11	112 N 4P -1	TA	-50	18						
17	6	103	S 4P +1	KK	450	91	22	9	108 S 3K +1	TD	130	41						
17	3	109	S 4P +1	K5	450	91	22	6	101 S 3K +1	TD	130	41						
17	1	105	S 4P +1	KK	450	91	22	7	104 S 3C =	PD	140	59						
18	6	103	S 2SA -1	K4	-100	5	22	4	109 S 3P =	TD	140	59						
18	9	110	S 3SA -1	PD	-100	5	22	3	107 N 3P +1	TA	170	73						
18	5	101	S 3T =	PD	110	18	22	10	110 N 4P =	TD	420	91						
18	8	108	N 3T +1	PA	130	36	22	8	106 N 4P =	TA	420	91						
18	7	106	S 3T +1	PD	130	36	22	12	102 S 4P =	TD	420	91						
18	10	112	S 3T +1	K4	130	36	23	10	109 S 3SA -2	P8	-200	0						
18	12	104	O 4K -3	CK	150	55	23	2	104 S 2SA -1	P10	-100	9						
18	3	109	S 1SA +4	K5	210	68	23	9	107 N 2T +1	P7	110	18						
18	1	105	S 2SA +3	K4	210	68	23	6	112 N 1SA +1	C6	120	36						
18	2	107	S 1SA +5	K4	240	82	23	5	110 S 1SA +1	P8	120	36						
18	4	111	W 3K X -2	TA	300	91	23	12	101 N 2SA =	C8	120	36						
18	11	102	S 3SA +2	K4	660	100	23	3	106 N 3T +1	K6	130	55						
19	6	102	S 4C +1	PK	450	0	23	8	105 N 2SA +1	C6	150	73						
19	9	109	S 4C +2	PK	480	50	23	7	103 S 2SA +1	P6	150	73						
19	8	107	S 4C +2	T5	480	50	23	1	102 N 2SA +1	C6	150	73						
19	7	105	S 4C +2	PK	480	50	23	4	108 S 2SA +2	C9	180	91						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.