

### Board-Anschriften (aus Sicht NS), Mitchell-Turnier Samstag - Hotel Hecht, Appenzell - 28.07.2018

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OWASpKonErgAus	Sco	Prz	Bd	NS	OWASpKonErgAus	Sco	Prz			
1	9	105	N 3SA -3	CK	-150	0	3	16	112 N 3K =	T4	110	70	6	3	103 W 2SA =	C2	-120	25
1	14	106	W 2C =	K9	-110	5	3	9	104 S 2C =	K9	110	70	6	18	117 O 2T +1	K5	-110	32
1	4	116	N 2SA -2	P6	-100	10	3	7	121 N 3K =	T6	110	70	6	4	114 O 3T =	PA	-110	32
1	1	101	N 2SA -1	C6	-50	15	3	6	119 N 2P =	TA	110	70	6	1	121 O 2T =	T4	-90	40
1	21	121	Pass		0	20	3	1	122 N 3P +1	TA	170	90	6	11	107 W 2SA -1	C2	100	58
1	18	115	W 3C -1	K8	50	28	3	11	108 N 3P +1	TA	170	90	6	15	111 O 2T -1	K5	100	58
1	7	122	W 2C -1	T10	50	28	3	8	101 N 3P +1	TA	170	90	6	14	109 W 3SA -1	C6	100	58
1	12	102	W 3C -2	K9	100	35	3	18	116 N 4P =	TA	420	100	6	9	102 O 3SA -1	T7	100	58
1	8	103	S 3K =	CB	110	42	4	17	114 W 3SA +1	T6	-630	2	6	6	118 W 3K -1	C2	100	58
1	3	114	S 3K =	CB	110	42	4	22	111 W 3SA +1	T6	-630	2	6	5	116 O 2SA -1	P10	100	58
1	20	119	N 2SA =	C6	120	55	4	20	120 W 3SA =	P10	-600	12	6	2	101 W 3SA -2	K9	200	80
1	5	118	N 2SA =	C6	120	55	4	15	110 W 3SA =	T6	-600	12	6	8	122 O 2P -2	T7	200	80
1	13	104	N 2SA =	P7	120	55	4	4	115 W 1SA +4	T3	-210	20	6	7	120 O 2SA -2	K4	200	80
1	6	120	S 2K +2	TD	130	65	4	16	112 W 1SA +3	T3	-180	30	6	19	119 W 3SA -3	KA	300	95
1	19	117	S 2SA +1	P2	150	75	4	9	104 W 1SA +3	T6	-180	30	6	12	104 W 3SA -3	K9	300	95
1	10	107	N 2SA +1	C6	150	75	4	6	119 W 2SA +2	P10	-180	30	6	22	112 W 2SA -3	C6	300	95
1	2	112	S 2SA +1	CB	150	75	4	1	122 W 3C +1	PB	-170	40	7	14	110 S 4C X -3	T4	-800	2
1	16	111	N 2P +2	C6	170	85	4	19	118 W 1SA +2	T6	-150	48	7	5	115 S 4C X -3	PK	-800	2
1	15	108	N 2SA +2	P4	180	90	4	14	107 W 1SA +2	T6	-150	48	7	4	104 S 4C -3	T4	-300	15
1	11	109	N 3SA =	CK	400	98	4	11	108 O 4K =	PA	-130	60	7	18	118 S 4C -3	T4	-300	15
1	22	110	N 3SA =	P6	400	98	4	10	106 O 4K =	PA	-130	60	7	2	122 S 4C -3	T4	-300	15
2	8	103	W 1SA +4	T7	-210	0	4	5	117 O 4K =	PA	-130	60	7	3	102 S 3C -2	T4	-200	30
2	19	117	W 2SA =	T7	-120	12	4	13	105 S 2P -1	T2	-100	72	7	1	120 S 3C -2	T4	-200	30
2	10	107	W 2SA =	T4	-120	12	4	21	109 S 3P -1	KA	-100	72	7	10	103 S 4C -2	T4	-200	30
2	12	102	W 1SA +1	T4	-120	12	4	2	102 O 5K -1	PA	100	82	7	15	112 S 3C -1	T4	-100	45
2	3	114	W 2SA =	T7	-120	12	4	7	121 O 4K -1	PA	100	82	7	8	121 S 3C -1	PK	-100	45
2	21	121	O 2C =	T2	-110	25	4	18	116 S 2P =	C5	110	90	7	19	107 S 4C -1	K7	-100	45
2	5	118	S 3P -1	TA	-100	30	4	8	101 W 3SA -3	PB	300	98	7	13	108 W 3P -1	C10	100	60
2	11	109	W 1SA =	T7	-90	42	4	12	103 W 3SA -3	T7	300	98	7	12	105 W 4K -1	C10	100	60
2	9	105	O 2T =	P4	-90	42	5	1	121 S 6SA -2	K4	-200	0	7	20	109 W 4K -1	C10	100	60
2	13	104	W 1SA =	T3	-90	42	5	14	109 N 1SA +4	T9	210	5	7	11	106 S 3C =	T4	140	72
2	2	112	W 2K =	P3	-90	42	5	4	114 N 3SA =	P5	600	10	7	7	119 S 3C =	T4	140	72
2	16	111	Pass		0	55	5	6	118 N 3SA +1	T9	630	15	7	9	101 S 2C +2	T4	170	80
2	18	115	O 4C -1	T2	50	65	5	20	108 N 5C =	T9	650	20	7	16	114 W 5K -2	C10	200	85
2	15	108	W 1SA -1	T6	50	65	5	19	119 N 3SA +2	T9	660	35	7	21	111 O 4P -3	CA	300	90
2	22	110	W 2SA -1	T7	50	65	5	18	117 N 5SA =	P2	660	35	7	6	117 W 5K X -2	TA	500	95
2	20	119	S 1P =	TA	80	78	5	17	115 N 3SA +2	P2	660	35	7	17	116 S 3C X =	P5	730	100
2	4	116	S 1P =	TA	80	78	5	10	105 S 3SA +2	K4	660	35	8	5	115 N 1P X -2	TK	-300	0
2	1	101	O 4C X -1	T2	100	90	5	5	116 N 3SA +2	P2	660	35	8	10	103 N 3SA -4	P10	-200	5
2	7	122	W 3K -2	PA	100	90	5	3	103 S 3SA +3	K4	690	72	8	16	114 O 2C +2	P7	-170	10
2	14	106	O 4K -2	P4	100	90	5	2	101 S 3SA +3	K4	690	72	8	1	120 N 3P -3	T9	-150	18
2	6	120	S 1P +1	TA	110	100	5	11	107 N 3SA +3	T9	690	72	8	19	107 N 2SA -3	T9	-150	18
3	2	102	W 3SA =	KK	-600	5	5	15	111 N 4SA +2	T9	690	72	8	18	118 O 2C +1	P7	-140	28
3	10	106	W 5T =	PA	-600	5	5	9	102 N 3SA +3	K5	690	72	8	6	117 O 2C +1	P7	-140	28
3	14	107	W 3SA =	C2	-600	5	5	13	106 S 3SA +3	K4	690	72	8	12	105 S 1SA -2	K9	-100	35
3	17	114	S 4C X -2	TK	-300	18	5	8	122 S 3SA +3	K4	690	72	8	4	104 O 2T =	P7	-90	40
3	22	111	N 4P X -2	CA	-300	18	5	12	104 S 3SA +3	K10	690	72	8	3	102 N 1P -1	TK	-50	62
3	13	105	N 4K -3	CA	-150	25	5	7	120 S 3SA +3	K9	690	72	8	17	116 N 1P -1	T9	-50	62
3	5	117	N 4P -2	CA	-100	30	5	21	110 S 3SA +3	K4	690	72	8	2	122 N 1P -1	T9	-50	62
3	19	118	N 3P -1	TA	-50	42	5	22	112 S 6SA =	K4	1440	100	8	15	112 N 3K -1	P4	-50	62
3	15	110	N 3C -1	TA	-50	42	6	10	105 W 3SA +1	KA	-630	0	8	14	110 N 1SA -1	P10	-50	62
3	12	103	S 2C -1	PK	-50	42	6	13	106 O 3T +2	P2	-150	5	8	13	108 N 1P -1	TK	-50	62
3	21	109	N 3P -1	CA	-50	42	6	17	115 O 2T +2	K10	-130	15	8	7	119 S 1SA -1	KB	-50	62
3	4	115	W 5T -1	PA	100	55	6	21	110 O 3T +1	K10	-130	15	8	20	109 N 2P -1	TK	-50	62
3	20	120	S 2C =	P10	110	70	6	20	108 O 3T +1	CA	-130	15	8	9	101 O 3C -1	P7	50	85

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
8	8	121	N 1P =	T9	80	92	11	9	121	W 2P =	T9	-110	45	14	9	120	W 1SA +1	P3	-120	8
8	21	111	N 1P =	TK	80	92	11	8	119	W 1P +1	T9	-110	45	14	7	107	W 1SA =	P3	-90	35
8	11	106	O 4C X -1	P7	100	100	11	15	114	S 3K -2	TA	-100	62	14	15	115	W 1SA =	P3	-90	35
9	17	117	W 4P X =	KK	-790	2	11	20	111	S 3K -2	C2	-100	62	14	5	103	W 1SA =	P3	-90	35
9	6	116	W 4P X =	KK	-790	2	11	16	116	W 2SA -1	K10	50	78	14	12	109	W 1SA =	P3	-90	35
9	22	114	N 3C X -2	P5	-300	10	11	14	112	W 3P -1	K5	50	78	14	11	102	W 1SA =	P3	-90	35
9	16	115	W 3P +2	KK	-200	18	11	2	120	W 3P -1	K7	50	78	14	10	122	W 1SA =	P3	-90	35
9	14	111	W 2P +3	KK	-200	18	11	18	107	W 3P -1	K10	50	78	14	18	108	W 1SA =	P7	-90	35
9	4	103	W 2P +2	K9	-170	28	11	6	106	W 3T -2	K10	100	95	14	8	118	W 1SA =	P3	-90	35
9	19	108	W 3P +1	KK	-170	28	11	12	108	W 4P -2	K10	100	95	14	16	104	W 1SA =	K4	-90	35
9	5	105	W 2P +1	KK	-140	40	11	1	118	W 4P -2	PB	100	95	14	3	121	N 2P -1	C3	-50	62
9	13	109	W 2P +1	C2	-140	40	12	14	112	W 4P +1	K3	-450	5	14	20	112	N 2SA -1	C3	-50	62
9	20	110	W 3P =	KK	-140	40	12	12	108	W 4P +1	C3	-450	5	14	6	105	O 1SA -1	T2	50	82
9	8	120	N 4K -2	P3	-100	52	12	11	103	W 4P +1	C10	-450	5	14	13	111	W 1SA -1	K4	50	82
9	18	106	N 4C -2	TA	-100	52	12	6	106	W 4P =	K3	-420	30	14	22	117	W 1SA -1	K4	50	82
9	11	104	N 5K -1	P6	-50	68	12	15	114	W 4P =	T8	-420	30	14	1	116	W 1SA -1	P3	50	82
9	9	122	N 3C -1	P6	-50	68	12	3	122	W 4P =	T6	-420	30	14	21	114	W 1SA -1	P3	50	82
9	21	112	N 3K -1	T2	-50	68	12	22	115	W 4P =	T6	-420	30	14	17	106	W 1T -1	K4	50	82
9	7	118	N 3C -1	P3	-50	68	12	10	101	W 4P =	K3	-420	30	14	2	119	W 2SA -2	P3	100	100
9	2	121	W 3P -1	KK	100	82	12	7	117	W 4P =	T8	-420	30	15	5	102	S 4C -1	K9	-100	0
9	10	102	W 4P -1	KK	100	82	12	17	105	W 4P =	T6	-420	30	15	4	122	S 2SA +3	P4	210	5
9	1	119	N 2C =	P3	110	90	12	16	116	N 3C -3	P2	-300	50	15	11	101	S 3SA =	P4	600	10
9	12	107	N 3C =	T8	140	95	12	1	118	W 3P =	T10	-140	55	15	14	114	S 4C =	K9	620	30
9	3	101	W 5P X -1	KK	200	100	12	5	104	W 4P -1	T6	50	72	15	6	104	S 4C =	K9	620	30
10	16	115	S 1SA -2	T2	-200	5	12	4	102	W 4P -1	T6	50	72	15	12	110	S 4C =	K9	620	30
10	13	109	S 2C -2	K7	-200	5	12	13	110	W 4P -1	K3	50	72	15	18	109	S 4C =	K9	620	30
10	9	122	S 2K -2	C4	-200	5	12	9	121	W 4P -1	C10	50	72	15	17	107	S 4C =	K9	620	30
10	4	103	N 1P -1	KA	-100	22	12	19	109	W 4P -1	T8	50	72	15	16	105	S 4C =	P4	620	30
10	2	121	S 1SA -1	T2	-100	22	12	8	119	W 4P -1	C3	50	72	15	15	103	S 4C =	K9	620	30
10	14	111	S 1SA -1	K7	-100	22	12	20	111	W 4P X -1	C10	100	92	15	13	112	S 3SA +1	P4	630	55
10	6	116	S 2K -1	T2	-100	22	12	18	107	W 4P X -1	C10	100	92	15	22	118	S 3SA +1	P8	630	55
10	7	118	Pass		0	35	12	2	120	W 4P X -2	C5	300	100	15	10	121	S 3SA +1	P4	630	55
10	5	105	S 1SA =	K7	90	48	13	4	101	O 4C +1	CK	-650	0	15	8	108	S 4C +1	P4	650	75
10	17	117	S 1SA =	TB	90	48	13	6	105	O 4C =	P10	-620	18	15	7	106	S 4C +1	K9	650	75
10	3	101	S 1SA =	K7	90	48	13	5	103	O 4C =	PK	-620	18	15	21	116	S 4C +1	P4	650	75
10	18	106	S 1SA =	KK	90	48	13	20	112	O 4C =	T3	-620	18	15	2	117	S 4C +1	K9	650	75
10	22	114	W 2K -1	K4	100	60	13	11	102	O 4C =	T6	-620	18	15	9	119	S 4C +1	P4	650	75
10	1	119	S 1SA +1	K7	120	72	13	19	110	O 4C =	PK	-620	18	15	1	115	S 3SA +2	P4	660	90
10	12	107	S 1SA +1	K7	120	72	13	8	118	O 4C =	T3	-620	18	15	3	120	S 4C +2	P4	680	98
10	8	120	S 1SA +1	K7	120	72	13	7	107	W 3C +1	K2	-170	42	15	19	111	S 4C +2	P2	680	98
10	20	110	S 1SA +1	C2	120	72	13	2	119	O 3C +1	PK	-170	42	16	13	112	W 2C +2	PA	-170	2
10	11	104	S 1SA +2	T10	150	88	13	10	122	O 3C +1	PK	-170	42	16	2	117	W 3C +1	T7	-170	2
10	19	108	S 1SA +2	KK	150	88	13	9	120	O 3C +1	P5	-170	42	16	14	114	W 2C +1	T6	-140	12
10	21	112	O 2C -3	PD	300	95	13	12	109	O 3C =	PK	-140	58	16	1	115	W 3C =	T10	-140	12
10	10	102	S1SAX+1	KK	380	100	13	1	116	O 3C =	K4	-140	58	16	6	104	W 2C =	T6	-110	28
11	10	101	S 3K X -3	C2	-500	2	13	15	115	O 4C -1	PK	100	80	16	19	111	W 2C =	T10	-110	28
11	7	117	N 2C X -3	P4	-500	2	13	3	121	O 4C -1	PK	100	80	16	11	101	W 2C =	K9	-110	28
11	22	115	S 3K -4	TA	-200	10	13	22	117	O 4C -1	PK	100	80	16	9	119	W 2C =	T10	-110	28
11	11	103	S 3K -3	C2	-150	18	13	21	114	O 4C -1	PK	100	80	16	12	110	W 3C -1	T7	100	58
11	17	105	S 3K -3	TA	-150	18	13	18	108	O 4C -1	PK	100	80	16	5	102	W 2C -1	T10	100	58
11	5	104	O 2C +1	PA	-140	28	13	17	106	O 4C -1	PK	100	80	16	4	122	W 3C -1	T6	100	58
11	19	109	O 3C =	PA	-140	28	13	16	104	O 4C -1	PK	100	80	16	3	120	W 2C -1	K9	100	58
11	4	102	W 2P =	K5	-110	45	13	13	111	O 6C -2	TD	200	100	16	21	116	W 2C -1	T10	100	58
11	3	122	W 2P =	T9	-110	45	14	4	101	W 1SA +2	KB	-150	0	16	18	109	W 3C -1	T10	100	58
11	13	110	W 3T =	K10	-110	45	14	19	110	W 1SA +1	C6	-120	8	16	17	107	W 3C -1	T6	100	58

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Samstag - Hotel Hecht, Appenzell - 28.07.2018**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
16	10	121	W 2C -1	T3	100	58	19	13	101	N 1SA =	K9	90	30	21	10	109	W 4C -3	P3	150	100
16	15	103	S 2P =	KK	110	80	19	9	108	S 1P +1	C2	110	40	22	7	103	O 3SA =	C8	-600	2
16	16	105	N 1P +2	C6	140	85	19	8	106	N 1SA +1	K9	120	52	22	16	108	O 3SA =	K4	-600	2
16	8	108	W 3C -2	T10	200	90	19	19	114	N 2SA =	T2	120	52	22	6	101	N 5K X -3	CA	-500	10
16	7	106	O 3SA -3	K2	300	95	19	17	109	N 1SA +1	K9	120	52	22	10	109	O 3T +1	K4	-130	15
16	22	118	W 3SA -5	T6	500	100	19	16	107	N 1SA +1	K4	120	52	22	22	121	S 3SA -2	TB	-100	22
17	14	102	N 5T =	K5	400	0	19	10	110	S 3P =	T5	140	75	22	5	120	S 4K -2	TB	-100	22
17	8	107	S 5T +1	KA	420	8	19	22	120	S 3P =	K2	140	75	22	21	119	N 4K -1	P4	-50	42
17	3	118	S 5T +1	KA	420	8	19	7	104	S 3P =	KA	140	75	22	20	117	N 4K -1	CA	-50	42
17	16	106	N 3SA +2	P10	460	15	19	18	111	S 2P +1	P3	140	75	22	3	116	N 3K -1	T7	-50	42
17	9	109	N 3SA +3	C4	490	45	19	3	117	S 2P +1	T5	140	75	22	14	104	N 3K -1	CA	-50	42
17	7	105	N 3SA +3	C5	490	45	19	21	118	N 1SA +2	P4	150	92	22	1	112	S 3K -1	TB	-50	42
17	6	103	N 3SA +3	C5	490	45	19	20	116	N 1SA +2	K8	150	92	22	12	122	N 3C -1	PD	-50	42
17	22	119	N 3SA +3	C5	490	45	19	11	121	S 4P =	T5	420	100	22	15	106	O 4T -1	C8	100	65
17	5	101	N 3SA +3	C5	490	45	20	2	115	W 4P +2	KK	-680	2	22	2	114	O 5T -1	K8	100	65
17	21	117	N 3SA +3	C5	490	45	20	14	103	W 4P +2	K5	-680	2	22	13	102	O 4T -1	C4	100	65
17	20	115	N 3SA +3	C5	490	45	20	5	122	W 4P +1	KK	-650	10	22	11	111	N 3K =	P4	110	80
17	19	112	N 3SA +3	C4	490	45	20	8	106	O 5T +1	KA	-620	25	22	8	105	N 3K =	CA	110	80
17	18	110	N 3SA +3	C5	490	45	20	19	114	O 5T +1	KA	-620	25	22	4	118	N 3K =	CA	110	80
17	1	114	N 3SA +3	C5	490	45	20	18	111	O 5T +1	KA	-620	25	22	17	110	O 5T -2	K4	200	90
17	17	108	N 3SA +3	K3	490	45	20	3	117	O 5T +1	KA	-620	25	22	9	107	W 3P -3	KA	300	98
17	12	111	N 3SA +4	C4	520	80	20	16	107	O 5T +1	KA	-620	25	22	19	115	W 3P -3	KA	300	98
17	4	121	N 3SA +4	C5	520	80	20	21	118	N 5K -4	TA	-400	40	23	3	115	S 5P -1	CA	-100	0
17	11	122	N 3SA +4	C5	520	80	20	15	105	S 4K -2	TB	-200	45	23	13	103	S 3P +2	CA	200	5
17	10	120	S 6T =	KA	920	90	20	10	110	O 3T +3	T4	-170	58	23	4	117	S 3P +3	CA	230	10
17	2	116	N 6SA =	C5	990	95	20	9	108	O 4T +2	C6	-170	58	23	21	120	S 4P =	CA	620	18
17	15	104	N 6SA +1	C5	1020	100	20	20	116	O 4T +2	KA	-170	58	23	6	121	S 4P =	CA	620	18
18	18	110	N 6C -3	TA	-300	0	20	13	101	O 3T +3	KA	-170	58	23	22	122	S 4P +1	CA	650	45
18	21	117	S 4P -1	T2	-100	8	20	22	120	N 3K -1	TA	-100	80	23	11	110	S 4P +1	CA	650	45
18	3	118	S 4P -1	K4	-100	8	20	7	104	N 4K -1	PD	-100	80	23	10	108	S 4P +1	CA	650	45
18	4	121	S 2P +3	T8	200	15	20	6	102	S 3K -1	TB	-100	80	23	9	106	S 4P +1	K2	650	45
18	22	119	N 3SA =	K3	600	20	20	17	109	S 3K -1	TB	-100	80	23	8	104	S 4P +1	CA	650	45
18	2	116	S 4P =	K4	620	35	20	11	121	N 3K -1	TA	-100	80	23	18	114	S 4P +1	CA	650	45
18	1	114	S 4P =	T8	620	35	20	4	119	S 2K =	C5	90	95	23	7	102	S 4P +1	CA	650	45
18	16	106	S 4P =	T8	620	35	20	12	112	N 3K =	TA	110	100	23	16	109	S 4P +1	CA	650	45
18	11	122	S 4P =	T8	620	35	21	4	118	W 2C +2	T10	-170	2	23	15	107	S 4P +1	CA	650	45
18	14	102	S 4P =	T8	620	35	21	13	102	W 2C +2	TK	-170	2	23	17	112	S 4P +2	T8	680	80
18	9	109	S 4P +1	C7	650	72	21	11	111	W 3C =	T2	-140	18	23	5	119	S 4P +2	K2	680	80
18	8	107	S 4P +1	C7	650	72	21	19	115	W 3C =	P9	-140	18	23	14	105	S 4P +2	CA	680	80
18	12	111	S 4P +1	T2	650	72	21	14	104	W 2C +1	T2	-140	18	23	12	101	S 5P +1	CA	680	80
18	7	105	N 4C +1	K7	650	72	21	1	112	W 1C +2	T2	-140	18	23	1	111	S 4P +2	CA	680	80
18	6	103	S 4P +1	T8	650	72	21	8	105	W 2C =	T2	-110	38	23	19	116	S 4P +3	C2	710	95
18	5	101	S 4P +1	T8	650	72	21	17	110	W 2C =	T2	-110	38	23	20	118	S 6P =	CA	1430	100
18	20	115	S 4P +1	T2	650	72	21	16	108	W 2C =	P3	-110	38	24	21	120	N 4C -1	P6	-50	8
18	19	112	S 4P +1	T8	650	72	21	2	114	W 2C =	T4	-110	38	24	17	112	N 3C -1	K4	-50	8
18	15	104	N 4C +1	K3	650	72	21	9	107	N 2P -1	CA	-100	50	24	14	105	N 4C -1	P6	-50	8
18	10	120	S 4P +1	CD	650	72	21	21	119	W 4C -1	TK	50	60	24	13	103	S 4C -1	PK	-50	8
18	17	108	S 4P +2	T8	680	100	21	7	103	W 3C -1	P3	50	60	24	9	106	W 5K -1	CA	50	22
19	12	112	S 4P -1	C2	-50	10	21	5	120	W 3C -1	K9	50	60	24	12	101	O 4P -1	CD	50	22
19	5	122	S 4P -1	P9	-50	10	21	22	121	N 1P =	T5	80	70	24	3	115	W 4P -2	CA	100	30
19	2	115	S 4P -1	P9	-50	10	21	20	117	W 4C -2	P3	100	82	24	10	108	N 3C =	KA	140	35
19	15	105	S 4P -1	T5	-50	10	21	6	101	W 4C X -1	TK	100	82	24	6	121	N 3C +1	K4	170	40
19	14	103	N 4P -1	K4	-50	10	21	15	106	W 4C -2	T2	100	82	24	16	109	W 4P X -2	CA	300	45
19	6	102	N 1SA =	T2	90	30	21	12	122	W 3C -2	T4	100	82	24	22	122	N 4C =	KA	420	60
19	4	119	N 1SA =	K4	90	30	21	3	116	N 2P =	C4	110	95	24	5	119	N 4C =	TA	420	60

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Samstag - Hotel Hecht, Appenzell - 28.07.2018**

Bd	NS	OW	ASpKonErgAus	Sco	Prz
24	15	107	N 4C =	P2 420	60
24	4	117	N 4C =	P5 420	60
24	1	111	N 4C =	KA 420	60
24	11	110	N 4C +1	KA 450	88
24	20	118	N 4C +1	KA 450	88
24	19	116	N 4C +1	P2 450	88
24	8	104	N 4C +1	TA 450	88
24	18	114	N 4C +1	KA 450	88
24	7	102	N 4C +1	TA 450	88